

herein incorporated by reference in its entirety.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

[0002] Not applicable.

BACKGROUND OF THE INVENTION

[0003] 1. Field of the Invention

[0004] The present disclosure is directed to a damper for mitigating blast waves in a duct.

[0005] 2. Background of the Invention

[0006] It is known that ignition of a flammable mixture in a duct may create a blast wave which propagates along the duct. This is a particular issue in oil or gas production platforms, where such flammable mixtures may arise. If such a blast wave propagates into a region where there are people, this may cause significant injury, such as burst eardrums or damaged lungs. The provision of louvers to inhibit such blast waves is known, but louvers cannot shut sufficiently quickly to prevent passage of the pressure wave.

[0007] Consequently, there is a need for a blast protection damper to prevent passage of pressure waves. Additional needs include the rapid closure of dampers to prevent passage of pressure waves.

BRIEF SUMMARY OF SOME OF THE PREFERRED EMBODIMENTS

[0008] According to the present disclosure there is provided a blast protection damper comprising a section of duct, with a multiplicity of substantially rigid elements each extending across the duct, the elements all extending parallel to each other and being arranged in an array consisting of a multiplicity of lines of said elements, each such line extending across the duct, the elements in one line being staggered relative to the elements in an adjacent line, and the gaps between successive elements within a line being no wider than the widths of the elements.

[0009] The damper is particularly suitable for ducts through which, in normal operation, there is a forced gas flow. For example, this may be a flow of air for cooling or for ventilation, and typically the flow velocity in normal operation is in the range between 1 and 5 m/s. The damper in the embodiment is to be distinguished from sound attenuators, as the elements in the blast damper are rigid and are not of a sound-absorbing or attenuating material. Such rigid materials may be characterised as those for which the characteristic acoustic impedance (the product of sound velocity and density) is greater than $10 \times 10^{10} \text{ kg m}^{-2} \text{ s}^{-1}$, and more preferably greater than $30 \times 10^{10} \text{ kg m}^{-2} \text{ s}^{-1}$. They may for example be tubes of steel or titanium or a titanium alloy.

[0010] Preferably the lines are straight lines, and within each line the elements are equally spaced. For example the lines may be columns extending between the bottom and the top of the duct. Preferably there are at least eight such lines of elements in the array, more preferably at least ten such lines, but preferably no more than fifteen. It will be appreciated that the more lines of elements are provided, the greater the pressure drop during normal use of the duct, so there is a disadvantage in providing excessive numbers of lines of elements. On the other hand, the more lines of elements are provided, the more effective the damper is at mitigating blast waves. The preferred number of lines appears to be about ten.

[0011] Preferably, the elements are of cylindrical shape, and the elements are preferably tubular, as this reduces weight while providing adequate strength. In a preferred embodiment the elements are tubes of diameter about 60 mm, and are arranged at center-to-center spacing's of no more than 120 mm, for example 100 mm so that the elements of a single column occupy about 60% of the projected area.

[0012] Preferably, the blast protection damper also includes a louver which is arranged to shut if the pressure in the duct exceeds a threshold. This may for example incorporate a mechanical latch arranged to hold the louver blades in an open position, but the louver blades being oriented such that the flowing gases within the duct urge the blades towards the closed position. If the pressure in the duct exceeds a threshold indicative of the presence of a blast wave, then the mechanical latch releases the blades, which move into the closed position under the combined effect of gravity and the gas pressure.

[0013] The foregoing has outlined rather broadly the features and technical advantages of the present invention in order that the detailed description of the invention that follows may be better understood. Additional features and advantages of the invention will be described hereinafter that form the subject of the claims of the invention. It should be appreciated by those skilled in the art that the conception and the specific embodiments disclosed may be readily utilized as a basis for modifying or designing other embodiments for carrying out the same purposes of the present disclosure. It should also be realized by those skilled in the art that such equivalent embodiments do not depart from the spirit and scope of the invention as set forth in the appended claims.

BRIEF DESCRIPTION OF THE DRAWINGS

[0014] For a detailed description of the preferred embodiments of the invention, reference will now be made to the accompanying drawings in which:

[0015] FIG. 1 illustrates a side elevation of a blast protection damper; and

[0016] FIG. 2 illustrates an end of view of the damper of FIG. 1 in the direction of Arrow 2.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0017] Referring to FIG. 1, a blast protection damper 10 forms part of a square duct 12 of width and height 1.2 m, through which the normal gas flow direction (and the potential blast wave direction) are indicated by Arrow A. The damper 10 consists of a section of square steel duct 14 which is of width and height 1.2 m, and of length 1.2 m, made of 5 mm-thick steel sheet, and connected to the duct 12 by means of flanges 16 at each end. There are 115 steel tubes 18 each of external diameter 60.3 mm and of wall thickness 3 mm which extend horizontally between opposite sides of the duct 14, being welded into corresponding holes in the sheets forming the duct wall, and being supported by corresponding holes in a vertical support plate 19 (shown in broken lines in FIG. 2) halfway across the duct 14. The tubes 18 are not indicated in FIG. 2, for clarity.

[0018] The tubes 18 are arranged in vertical columns, within each column the tubes 18 being spaced apart center-to-center (y) at 100 mm, and the longitudinal distance (x) between the centers of successive columns also being 100 mm. There are twelve tubes 18 in the first column, so that the gaps between adjacent tubes are about 40 mm, and similarly there are gaps of about 20 mm between the top and bottom tubes 18 and the top and bottom walls of the duct 14. The arrangement of the tubes in the other odd-numbered columns is identical to that in the first column. The even-numbered columns each have eleven tubes 18, and the tubes 18 are staggered relative to those in the odd-numbered columns, so that the centers of the tubes 18 are exactly midway in height between those of the tubes in the odd-numbered columns.

[0019] At the downstream end of the array of tubes 18 is a louver mechanism 20, consisting of eight louver blades 22 (shown in broken lines in FIG. 1) which in normal operation (as shown) are oriented at about 45.degree., each of length about 190 mm, whose upper edge is fixed to a 25 mm diameter steel rod 24. The steel rods 24 extend through bearings in the side walls of the duct 14, and are welded to arms 25 all of which are pivotally connected to a link bar 26. The link bar 26 is secured by a spring-operated latch mechanism (not shown) in a box 27, such that if the pressure forces acting on the blades 22 exceeds a threshold value, then the latch is released, so that the blades 22 rotate into a generally vertical position, under the effect of both the gas pressure and gravity. In the resulting, closed, position of the louver mechanism 20 the bottom edge of each blade 22 rests against the steel rod 24 of the next blade down, apart from the lowest blade 22 which rests against a stop 28.

